Seismic Assessment of RC Building Using Pushover Analysis

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Abstract: Current research works indicated that parts of Kingdom of Saudi Arabia have low to moderate seismic regions. For structural engineers, seismic load should be considered as important aspect that needs to be included in the building design. However Major part of buildings are designed for gravity loading only and poorly detailed to accommodate lateral loads. The purpose of this paper is to investigated gravity supporting building its resistance to expected seismic loading in different regions (Makkah, Jeddah, Gizan and Haql).

In this paper, a test RC building that was designed for gravity loading only is investigated. This will be accomplished by performing the nonlinear static analysis (pushover analysis) according to ATC 40. Pushover analysis produces the pushover curves, capacity spectrum, plastic hinges and performance level of the building. This analysis gives better understanding seismic performance of buildings and also traces the progression of damage or failure. The building performance level is determined by intersection of demand and capacity curves and the hinge developed in the beams and the columns. The results show that the test building is found inadequate for Haql region and it still can be considered for Makkah, Jeddah and Gizan.

Keywords— seismic analysis; pushover; ATC 40; seismic zone; capacity spectrum

Introduction

The Kingdom of Saudi Arabia lies within low to moderate seismic region. Seismic load should be considered as important aspect that needs to be included in the building design. In the past decades, the inclusion of dynamic loads in the design of building in Saudi Arabia was very much limited to important huge structures. Recently, the development and adoption of a national code and the experienced seismic activity at several regions in the Kingdom necessitate the detailed consideration of seismic loads in the design of all buildings. Major part of building industry are designed for gravity loading only and poorly detailed to accommodate lateral loads. The existing buildings have to be provided by some rehabilitation to sustain the expected performance level. The capacity of the building should be evaluated before rehabilitation work [4].

It is generally believe that the conventional elastic design analysis

method cannot capture many important the that control seismic aspects performance of the building. The capacity building undergo inelastic to of deformations governs the structural behaviour of building during seismic ground motions. For that reason, the evaluation of building should be based the deformation demanded inelastic bv seismic. On the other hand, linear elastic analysis does not provide information about real strength, ductility and energy dissipation [5].

Nonlinear dynamic analysis is principally correct approach. However, it is very complex and not practical for every design. It needs time history of ground motion data and detailed hysteretic behaviour of structural members which cannot be predicted. This analysis is appropriate for research and for design of important structures [11].

For estimating seismic demands for building, the structural engineering profession is now using the non-linear 2nd International Conference on Engineering and Technology Development (ICETD 2013) Universitas Bandar Lampung

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static procedure, known as pushover analysis. It is a commonly used technique, which is finding prominence in standards and guidance material. The term static implies that a static method is applied to represent a dynamic phenomenon [6].

Pushover analysis is a series of incremental static analysis carried out to develop a capacity curve for the building. Figure 1 illustrates pushover analysis. This procedure needs the execution of a nonlinear static analysis of structure that allows monitoring progressive yielding of the structure. The building is subjected a lateral load. The load magnitude increase until the building reaches target displacement. This target displacement is determined to represent the top the building is displacement when subjected design level to ground excitation.



Fig. 1 Illustration of Pushover Analysis [ATC 40]

Pushover analysis produces pushover curve or capacity curve that presents relationship between base shear (V) and roof displacement (Δ). The Pushover curve depends on strength and deformation capacities of the structure and describes how the structure behaves after the elastic limit.

Structural response to ground motion during earthquake cannot be accurately predicted due to the complexity of the structural properties and ground motion parameters. In pushover analysis, a set of lateral displacement is used directly as design condition. The displacement is an estimate of the maximum expected response of the structure during ground motion.

Once pushover analysis is defined, the performance level can be

determined using demand displacement. The performance verifies the structure is adequate the acceptable limits of performance level.

Recently, there are some codes such as ATC-40, FEMA 256, FEMA 440 adopted standards and guidance materials regarding the assessment of existing structures. Some programs are also developed for pushover analysis and are listed: SAP2000, ETABS, and DRAIN-2DX.

A. Capacity Spectrum

Building performance level can be determined by target displacement using capacity spectrum method (ATC 40). The capacity spectrum method allows for a graphical comparison between the structure capacity and the seismic demand. Pushover curve represents the lateral resisting capacity and response spectrum curve represents the seismic demand.

The capacity spectrum method, which is given in Figure 2, is started by producing force-displacement curve that consider inelastic condition. The result is then plotted to ADRS (Acceleration Displacement Response Spectrum). Demand is also converted into ADRS format so that capacity curve and demand curve are in the same format [1].





The performance point is obtained by superimposing demand spectrum on

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capacity curve into spectral coordinate or ADRS format. The capacity spectrum method has been built in SAP2000 program

Performance levels of buildings are shown in table I

TABLE

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PERFORMANCE LEVEL OF BUILDING

4											
	Level	Description									
	Operational	Very light damage, no permanent drift,									
		structure retains original strength and									
		stiffness, all systems are normal									
	Immediate	Light damage, no permanent drift,									
	Occupancy	structure retains original strength and									
		stiffness, elevator can be restarted, Fire									
		protection operable									
	Life Safety	Moderate damage, some permanent drift, some residual strength and stiffness left in									
		all stories, damage to partition, building									
		may be beyond economical repair									
	Collapse	Severe damage, large displacement, little									
	Prevention	residual stiffness and strength but loadin									
		bearing column and wall function, building									
		is near collapse									

B. Nonlinear Plastic Hinge

Pushover Analysis requires the development of the force-deformation curve for the critical section of beams and column by using the guideline [3]. Such a curve is presented in Figure 3



Fig. 3 Typical load-deformation relation and target performance level

Point A corresponds to the unloaded condition. Load deformation relation shall be described by linear response from A to an effective yield B. Then the stiffness reduce from point B to C. Point C has resistance equal to the nominal strength then sudden reduction in lateral load resistance to point D, the response at reduced resistance to E, final loss of resistance thereafter. The slope of line BC, ignoring effects of gravity effects of gravity loads acting through lateral displacement, is usually taken between 0 and 10% of the initial slope. Line CD corresponds to initial failure of the member. Line DE represents the residual strength of the member.

These points are specified according to FEMA to determine hinge rotation behaviour of RC members. The points between B and C represent acceptance criteria for the hinge, which is Immediate Occupancy (IO), LS (Life Safety), and CP (Collapse Prevention).

I. DESCRIPTIVE OF THE TEST BUILDING

The test building is a 3-story reinforced concrete building, with height story 4.0 m. The overall plan dimension is 21 x 15 square meters. Figure 3 shows the typical structural layout. Beam 1 is 700/400 and Beam 2 is 500/300 mm square for all stories. The columns are rectangular 500/300 mm. Type of soil is soft rock or site class C according to Saudi Building Code 301.



Fig. 4 Structural Layout

The structural system was designed for supporting gravity load only. Longitudinal bar in beams are bent upwards at their end to resist negative moment due to gravity load. Strong lateral load can change the moment at the end span of the beam. Therefore, the bottom Faculty of Engineering and Faculty of Computer Science

steel at end of the beam may be not adequate for lateral load. Summary of modelling assumption is presented in Table II.

TABLE II Modelling Assumption

÷		C I			
	Material				
	Concrete	4000psi			
	Steel	A615Gr60			
	Loading				
	Self-weight	Automatically by Software			
	Dead load	2.7 kN/m ²			
	Live Load	2.5 kN/m ²			
	Wind Load	Not Considered			
	Modelling				
	Element	Linear element for beam and column			
		Shell element for slab			
	P-delta effect	Not considered			
	Diaphragm	Shell element for slab			
	Support	Fixed			

II. PUSHOVER ANALYSIS

In the present paper, Pushover analysis is carried out using SAP2000 program. A three dimensional model of structure has been created as shown in Figure 5.



Fig. 5 Pushover Curve for X and Y Direction

Beams and columns are modelled as nonlinear frame element at the start and the end of element. The FEMA 356 rule, which is built in SAP 2000 with the IO, LS, and CP limit states for hinge rotation have been used for the acceptance criteria. The pushover analysis is executed separately for two orthogonal directions to study the performance of the building in both directions. Gravity push, which is applied for gravity load only, Push-X is the lateral push for X direction starting at the end of gravity push, Push-Y is for Y direction starting at the end of gravity push.

The pushover analysis is achieved using a displacement control strategy, where the building is subjected the lateral load pattern until the roof displacement reach a target value. The minimum number of state used is 10 and the maximum is 100.

Pushover analysis is performed in four different regions in KSA (Makkah, Jeddah, Gizan, and Haql). Parameters Ca and Cv are taken from Saudi Building Code 301 to construct response spectrum curve as shown in figure 6.



Fig. 6 Response Spectrum Curve for Each Region

III. RESULT OF ANALYSIS

Pushover curves for the building for X and Y direction are presented in Figure 6. These curves represent the global behavior of the frame in terms of stiffness and ductility. Under incrementally increasing lateral load, the structural element may be vield sequentially. At every step, the structure experience loss in stiffness. Therefore, slope of pushover curve gradually is decreasing.

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The comparison of pushover curve in X and Y direction shows that the stiffness of frame is more in X direction as compared to Y direction. This is explained that Y-direction is the critical point.



Fig. 7 Pushover Curve

The performance point has been obtained by superimposing demand spectrum on capacity curve into spectral coordinate. Figure 8 shows capacity spectrum for Gizan region in X direction. It is obvious that the demand curve tend to intersect the capacity curve at the performance point. For Gizan, It can be concluded that there are sufficient strength and displacement reserves at this performance point.



Fig. 8 Capacity Spectrum

Table III summarizes the performance point of the structure for each region.

TABLE

PERFORMANCE POINT FOR EACH REGION

	X-I	Direction	L	Y-Direction		
	V	d	step	V	d	step
Mekkah	675.10	0.015	2	518.84	0.021	2
Jeddah	966.48	0.026	3	633.63	0.034	5
Gizan	1014.27	0.029	4	641.26	0.039	6
Haql	1155.06	0.069	7	691.31	0.110	9

At every deformation step of pushover analysis determine plastic rotation hinge location in the elements and which hinges reach the FEMA limit state, which are IO, LS, and CP using colours for identification.

Plastic hinges formation have been obtained at different displacement levels or performance points. The hinging patterns for each region are plotted in figure 7.

Makkah

The element response is still not dangerous at this performance point. Yield occurs in some elements but none of them exceeds IO (Immediate Occupancy) level. The outer columns still behave in elastic range.

Jeddah

Most of elements are in yield condition. The damage of the building is still limited both in X and Y direction since yielding occurs at event B (yielding) to IO (Immediate Occupancy).

Gizan

Although the element response is generally adequate at this performance point, the response is more severe in Ydirection. The yielding at the lower column occurs at event IO (Immediate Occupancy) to LS (Life Safety).

Haql

For X direction, the building is still adequate due to yielding occurs at even B to IO. However, the building is not adequate for Y direction due to the lower columns yield exceed C (Collapse) condition.

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Fig. 9a Deformed Shape of the Frame-2 for Makkah (X-Dir)



Fig. 10b Deformed Shape of the Frame-2 for Jeddah (X-Dir)



Fig. 11c Deformed Shape of the Frame-2 for Gizan (X-Dir)



Fig. 12d Deformed Shape of the Frame-2 for Haql (X-Dir)



Fig. 13e Deformed Shape of the Frame-2 for Makkah (Y-Dir)



Fig. 14f Deformed Shape of the Frame-2 for Jeddah (Y-Dir)



Fig. 15g Deformed Shape of the Frame-2 for Gizan (Y-Dir)



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Fig. 16h Deformed Shape of the Frame-2 for Haql (Y-Dir)

IV. CONCLUSION

The test building is investigated using pushover analysis. These are conclusion obtained from this analysis:

- 1. Pushover analysis is a simple way to investigate nonlinear behavior of the building. The result obtained gave an understanding into nonlinear behavior, which is real behavior of structure.
- 2. Pushover analysis is approximation method and based on static loading. It may not accurately represent dynamic phenomena.
- 3. The performance level of structure is indicated by intersection of demand and capacity curves and the hinges developed in the beams and the columns.
- 4. The results show the building that was designed only for gravity load is found inadequate for Haql region. However, the building still can be considered for Makkah, Jeddah and Gizan.
- 5. Pushover analysis can identify weak bv predicting elements failure mechanism and account for redistribution of forces during progressive yielding. It may help engineers make action for rehabilitation work.

REFERENCES

- 1. Applied Technology Council, Seismic Evaluation and Retrofit of Reinforced Concrete uildings", Report ATC 40 /, 1996.
- 2. The Saudi Code National Building Committee, *The Saudi Building Code 301 Structural – Loading and Forces*, 2007.
- 3. American Society of Civil Engineers, FEMA-356: Prestandard and Commentary for The Seismic Rehabilitation of Buildings, 2000.

- Attar, M. S, "Evaluation of the Seismic Performance of A Typical School Building" Master Thesis, College of Engineering, KAAU, 2003.
- Abd-alla, Mohamed N, "Application of Recent Techniques of Pushover for Evaluating Seismic Performance of Multistory Building" Faculty of Engineering, Cairo University, 2007
- Giannopoulos, P.I 6. "Seismic Assessment RC Building of according to FEMA 356 and Eurocode 8" 16th Conference on Concrete, TEE. ETEK. 21-23/10/2009
- Vijayakumar, A and Babu, D.L.V. "Pushover Analysis of Existing Reinforced Concrete Framed Structures" European Journal of Scientific Research, ISSN 1450-216X Vol.71 No.2 (2012), pp. 195-202
- Chopra, A.K and Goel, R.K "A Modal Pushover Analysis Procedure to Estimate Seismic Demands for Unsymmetric-plan Buidings" Earthquake Engng Struct. Dyn. 2004; 33 :903–927 (DOI: 10.1002/eqe.380)
- Elnashai, A.S. "Advanced inelastic static (pushover) analysis for earthquake applications" Structural Engineering and Mechanics, Vol 12, No. 1, 2001
- Poluraju, P and Rao, N. "Pushover Analysis of reinforced concrete frame structure using SAP 2000" International Journal of Earth Science and Engineering ISSN 0974-5904, Volume 04, No 06 SPL, October 2011, pp. 684-690
- 11. Fajfar, P. "Structural Analysis in Earthquake Engineering – Breakthrough of Simplified Nonlinear Methods" 12th European Conference on Earthquake Engineering, Paper References 843